

# Numerical Simulation of Acoustic Effects of Engine Installation for New Concepts of Aircrafts

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*“Aeroacoustics of New Aircraft & Engine Configurations”*  
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# Context



- \* *Future aircraft projects*
- \* *Engine noise shielding by airframe*
- \* *Numerical simulation*

# Tools for numerical simulation of acoustic shielding effects

## Noise source modeling

- Engine noise sources (fan, jet) are very complex
- Interesting results can be obtained by using simplified source : distribution of monopoles

## Noise prediction

### Acoustic propagation simulation

May include effects of :

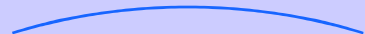
- Scattering on complex solid bodies
- Refraction through non-uniform mean flows

# In-house solvers developed at *ONERA*

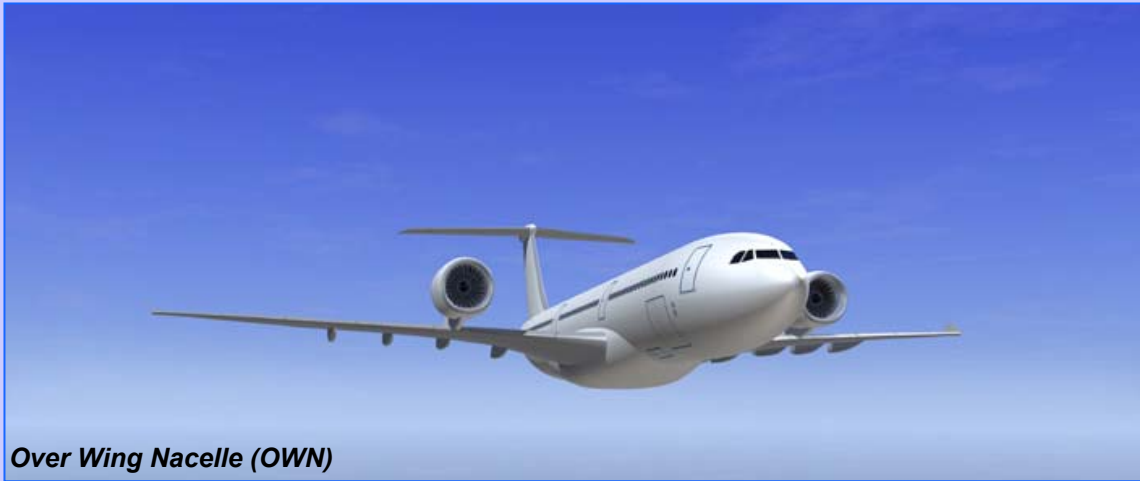
	<b><i>BEMUSE</i></b>	<b><i>sAbrinA</i></b>
Solved equation(s)	<b>Helmholtz</b>	<b>Euler (in perturbation form)</b>
Numerical method	<b>Boundary Element Method Variational formulation</b>	<b>Finite difference, high order spatial schemes and filter</b>
Grid	<b>Body surface Unstructured</b>	<b>Fluid Structured</b>
Scattering effect on rigid bodies	<b>Yes</b>	<b>Yes</b>
Refraction effects through non uniform flow	<b>No flow (uniform flow under progress)</b>	<b>Yes</b>

# In-house solvers developed at *ONERA*

## *Part I : BEMUSE code*

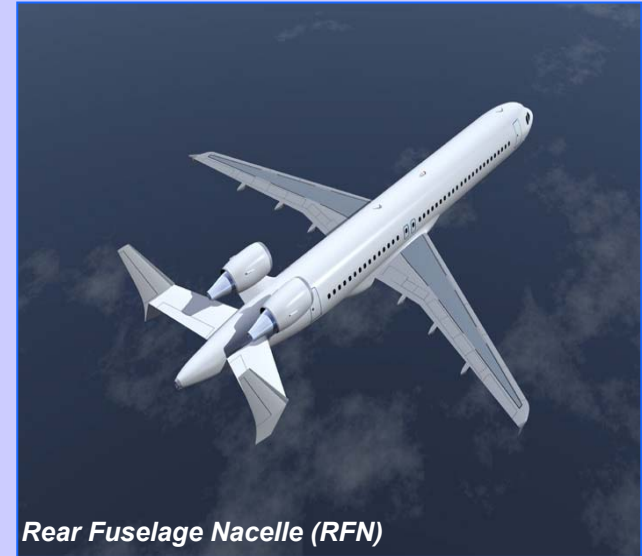


# BEMUSE solver : Context of design



*Over Wing Nacelle (OWN)*

**European Project ROSAS (Research On Silent Aircraft conceptS)**



*Rear Fuselage Nacelle (RFN)*

**ONERA's objectives in task 3.3.3 (« Numerical work »):**

- \* *Fuselage, wing and empennage shielding effects assessment*
- \* *Acoustic scattering from distribution of point sources*
- \* *Geometry : ROSAS aircraft, scale 1:1 Model with up to 100,000 Degrees Of Freedom (DOF)*
- \* *Frequency : up to fan blade passing frequency (BPF)*
- \* *Running on parallel PC Cluster (powerful / cheap)*

**Code design :**

- \* *Parallel BEM (Boundary Element Method) code*
- \* *Built from existing BEM modules (electromagnetism)*
- \* *Computer : ONERA's PC Cluster : 32 biprocessor PCs*



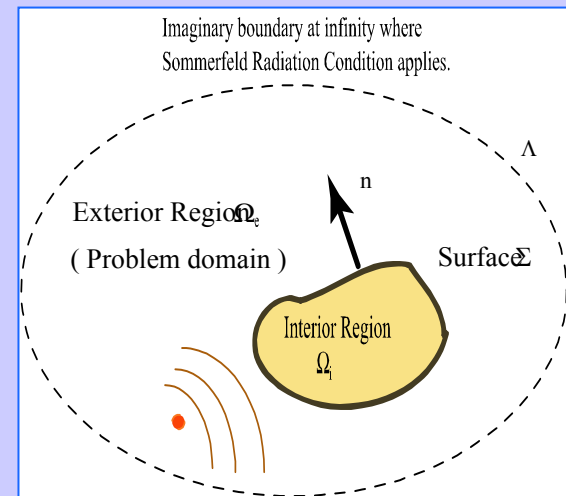
ONERA

# Boundary Element Method

**Helmholtz equation**  $\Delta p(x) + k^2 p(x) = 0 \quad \left( k = \frac{\omega}{c} \right)$

**Rigid boundary condition on  $\Sigma$**   $\frac{\partial p}{\partial n} = 0, x \in \Sigma$

**Sommerfeld radiation condition on  $\Lambda$**



**Integral solution using a free-space Green function**

$$\int_{\Sigma} \left[ p(y) \frac{\partial G(x, y)}{\partial n} - \frac{\partial p}{\partial n}(y) G(x, y) \right] dy = \begin{cases} p(x) & x \in \Omega_e \\ \frac{1}{2} p(x) & x \in \Sigma \\ 0 & x \in \Omega_i \end{cases} \quad G(x, y) = \frac{e^{-ik\|x-y\|}}{4\pi\|x-y\|}$$

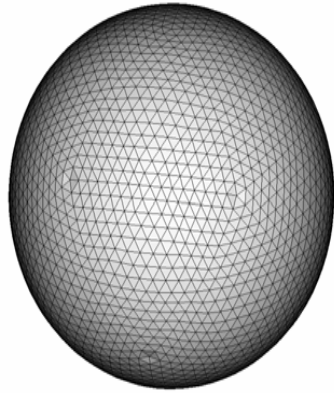
**Discretization using a shape function  $[N]$  to interpolate  $p$  and its derivative on  $n$  DOF on  $\Sigma$**

$$\frac{1}{2} p(x) = \sum_{i=1}^n \int_{\Sigma} \frac{\partial G(x, y)}{\partial n} [N] dy \{p(x_i)\} - \sum_{i=1}^n \int_{\Sigma} G(x, y) [N] dy \left\{ \frac{\partial p}{\partial n}(x_i) \right\}$$

**Set of  $n$  linear equations :**  $[H]\{p\} = -[G]\left\{ \frac{\partial p}{\partial n} \right\}$   **$[H]$  and  $[G]$  are  $n \times n$  symmetric plain matrices**

## BEM computations

- 1) BEMUSE code on PC (1 node)
- 2) SYSNOISE code on UNIX workstation



Unstructured grid :  
2562 DOF

## Analytical solution

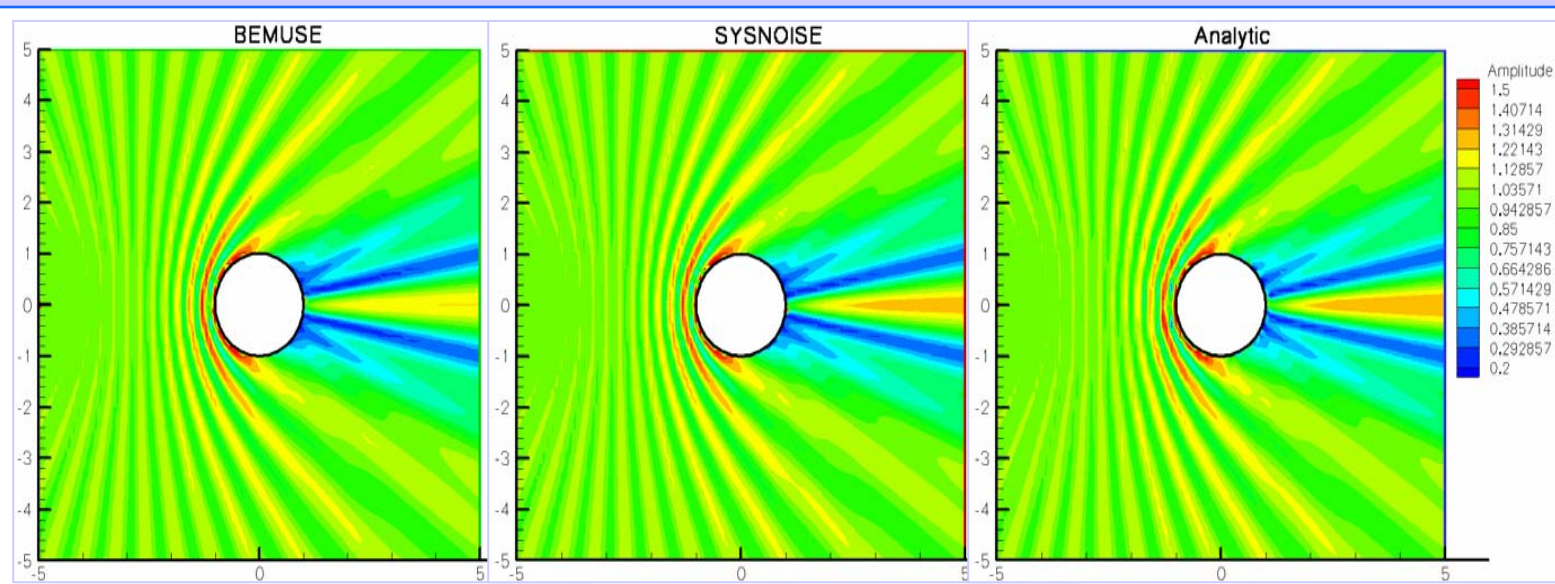
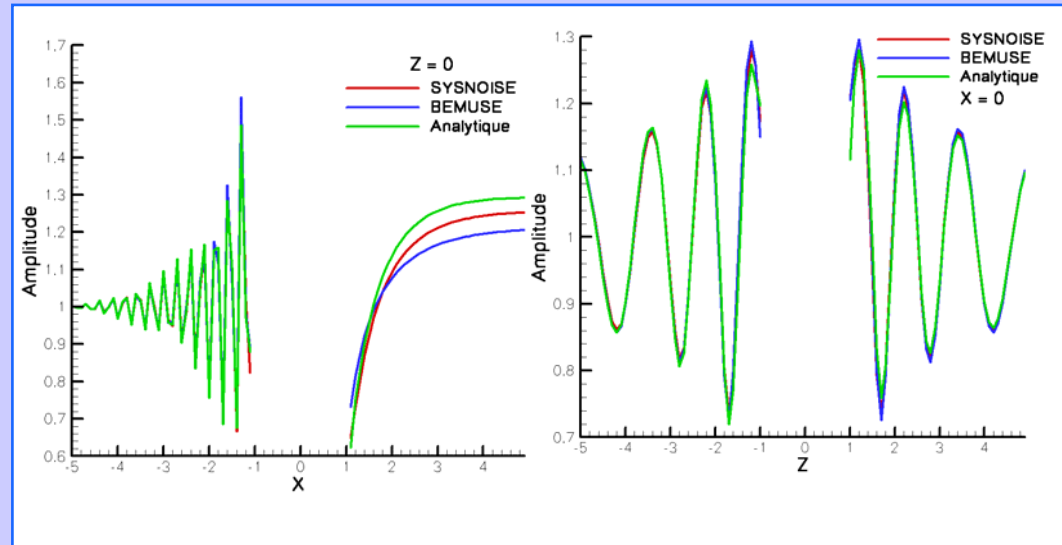
$$(r, \theta, \varphi) = \sum_{l=0}^{+\infty} \sum_{m=-l}^{+l} v_l^m \frac{h_l^{(1)}(kr)}{k \frac{\partial}{\partial r} h_l^{(1)}(k)} Y_l^m(\theta, \varphi)$$

## BEMUSE validation

Acoustic scattering on a rigid sphere :  $r = 1$

Incident spherical wave : frequency = 600 Hz

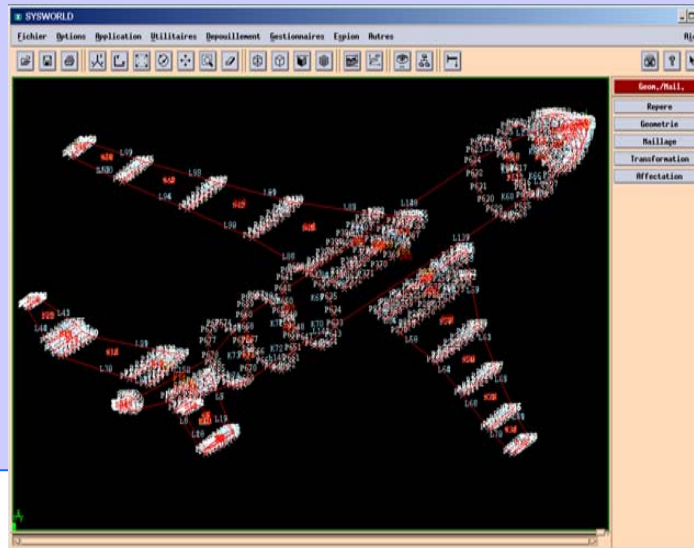
Normalized frequency  $kr = 11$





# Grid construction

- *ROSAS aircraft UWN, OWN, RFN*
- *Up to 110,000 DOF*
- *Simplified but realistic shape*
  - *Analytical sections*
  - *Direct junction wing/fuselage*

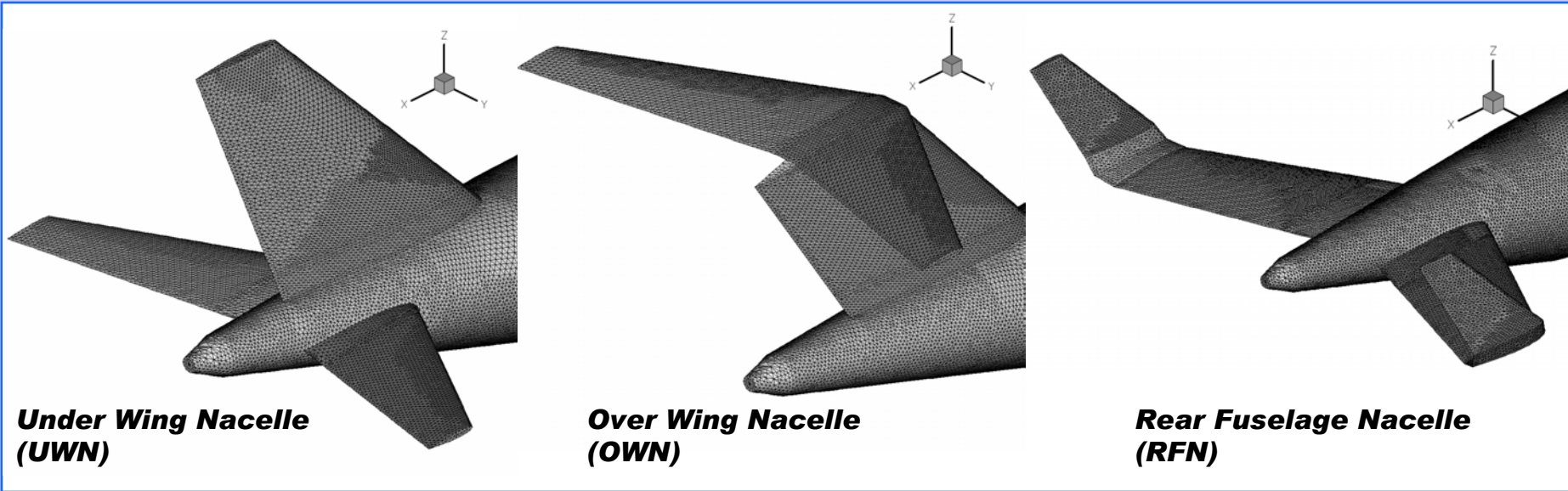


**SYSTUS software**



**Reference configuration :  
Under Wing Nacelle (UWN)**

# Grid details of the empennage region



## Early computations

- \* Mid-size grids : 30,000 DOF, UWN, OWN, RFN
- \* Low frequency : 150 Hz

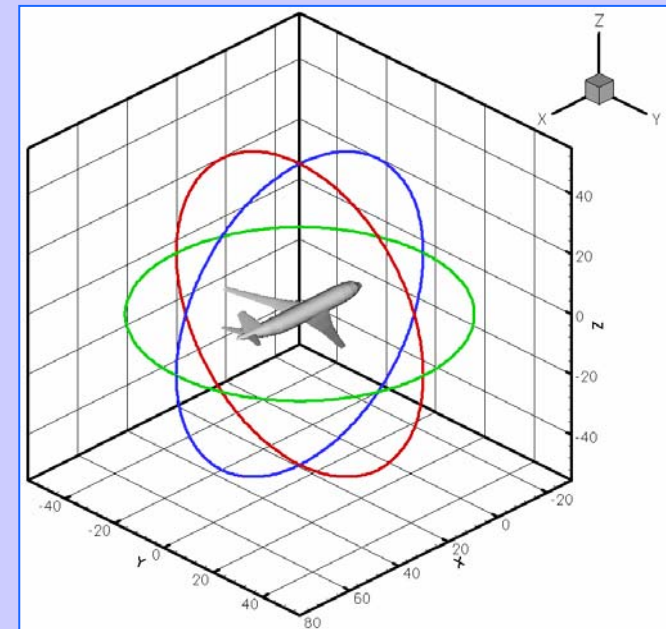
## Results

### Pressure distribution at aircraft surface

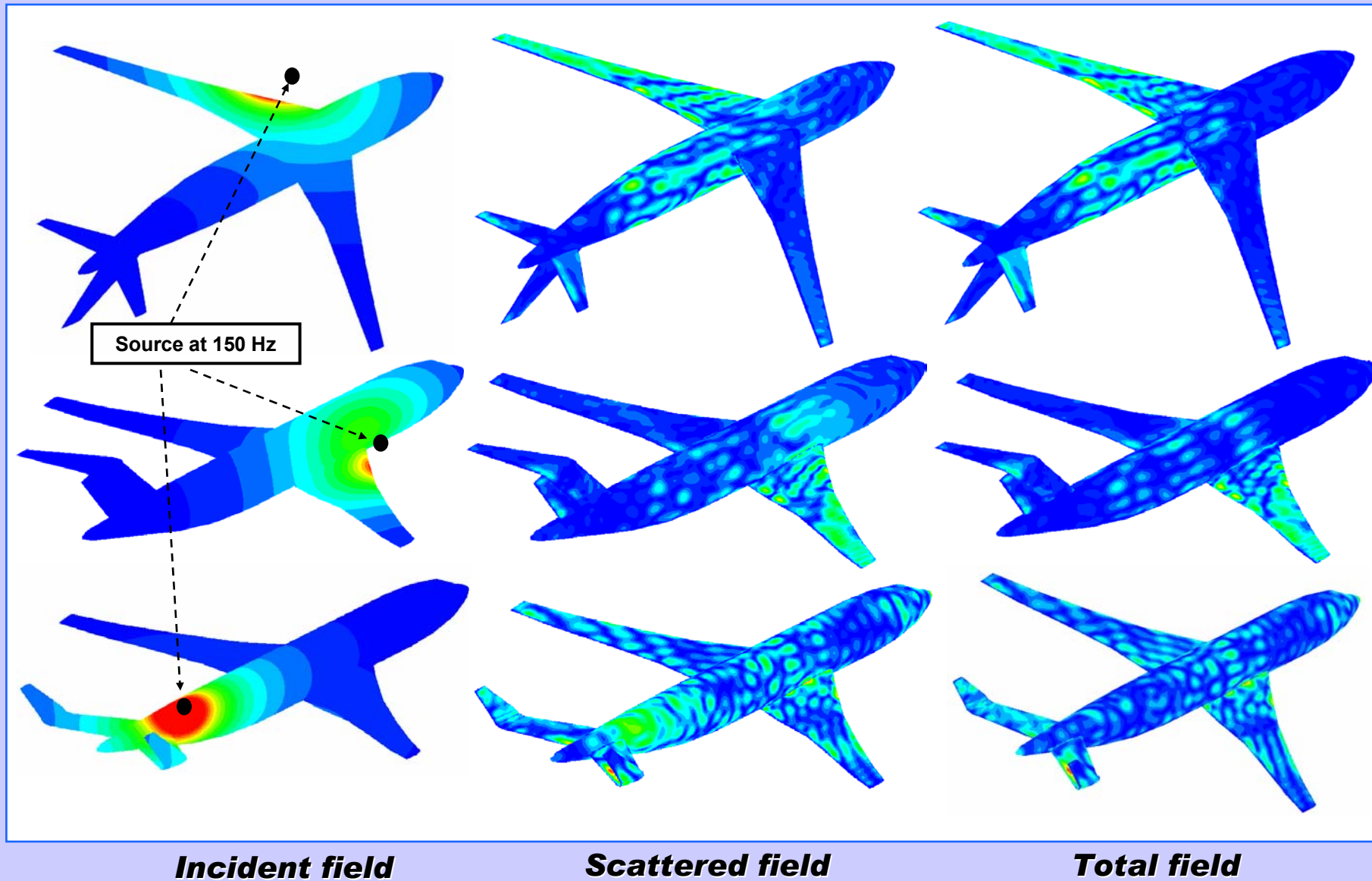
- Incident, scattered, total fields

### Directivity diagrams

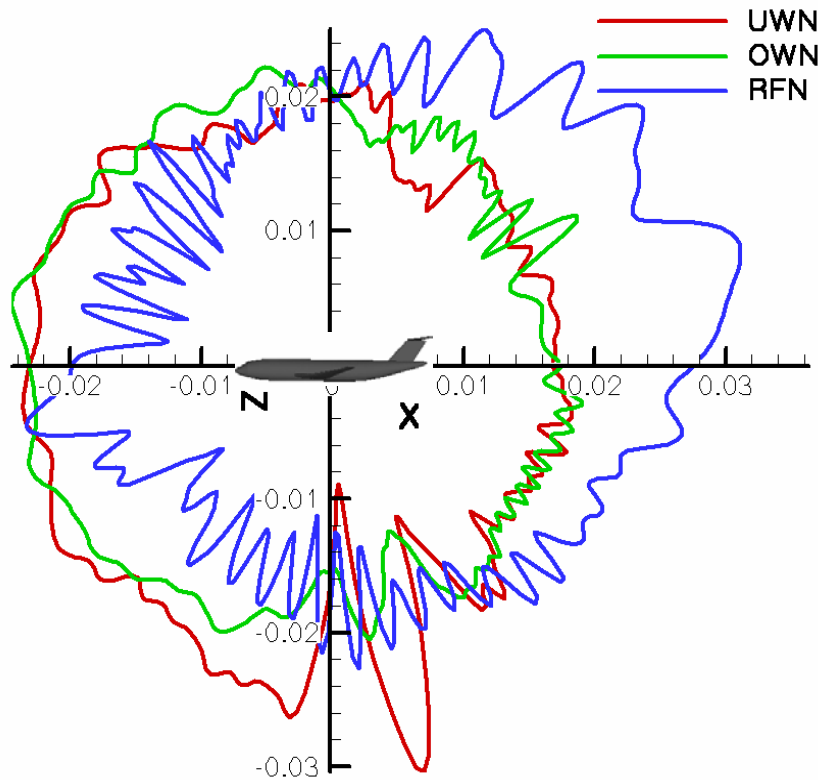
- Circles in XY, XZ and YZ planes
- Centered at fuselage center  $X = 25$  m
- Mid-field :  $R = 50$  m (one fuselage length)



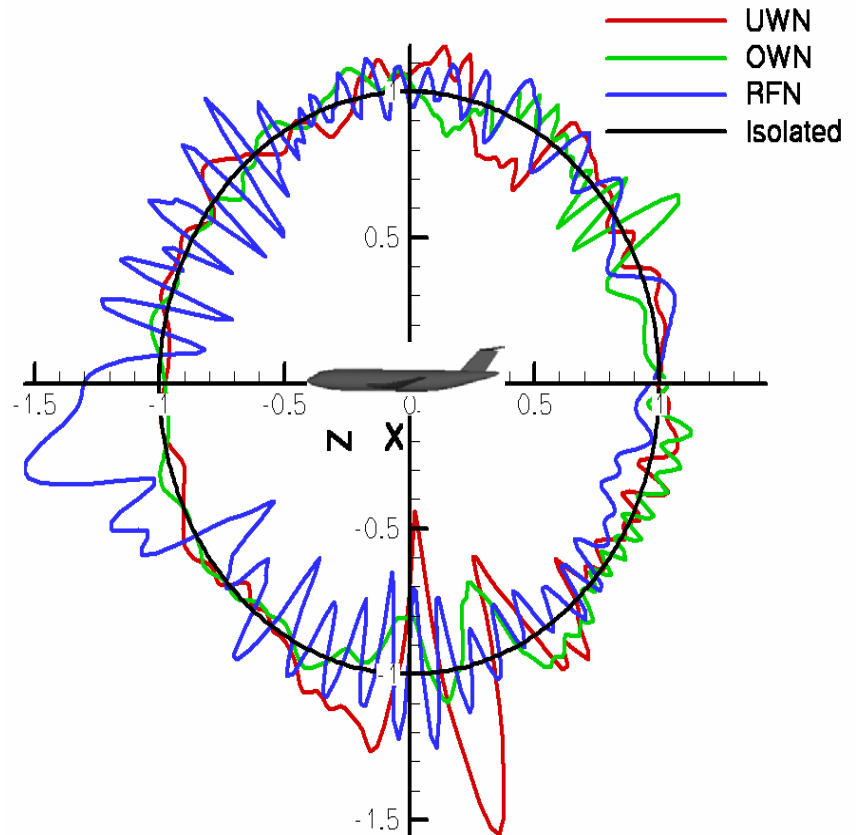
Results: Pressure distribution at aircraft surface



## Results : Directivity diagrams in the ZX plane ( $r = \text{one fuselage length}$ )



*Not corrected from the  
distance source-observer*

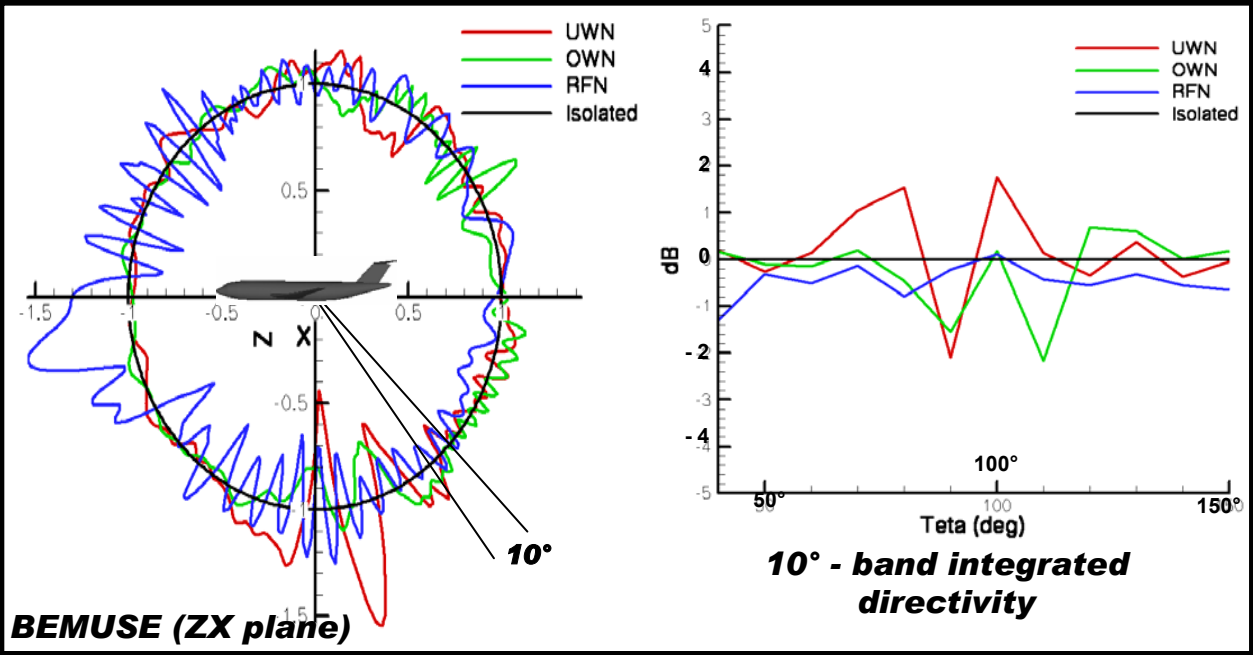
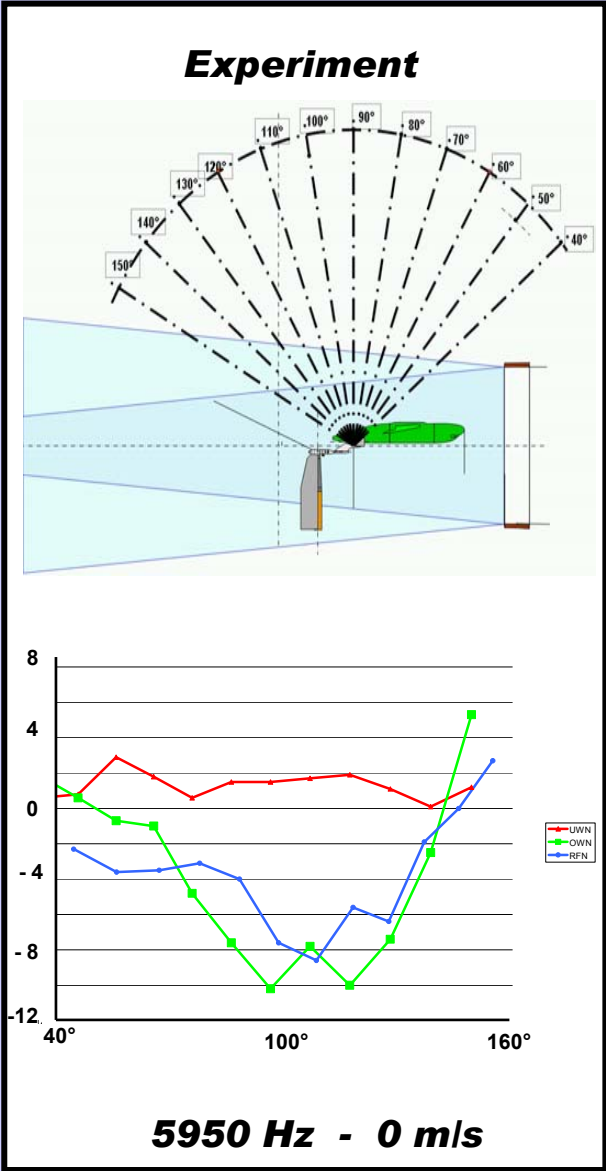


*Corrected from the  
distance source-observer*



Results : Tentative of comparison with CEPRA 19 experiments (ROSAS campaign)

	BEM computation	Experiment
Aircraft	ROSAS Aircraft	Airbus aircraft
Scale	1:1	1:11 (1:16 w.r.t. ROSAS A/C)
Source	Monopole (at the engine inlet)	TPS (certainly not spherical)
Frequency	150 Hz (→ 2.4 kHz at 1:16)	6 kHz
Observer	R = 50 m (one fuselage length)	R = 6 m (two fuselage lengths)



## *Application of BEMUSE to installation effects studies : Next steps*

- ❑ Computations on larger grids (110,000 DOF) and at higher frequencies (under progress)
- ❑ Grids :
  - half - grids (aircraft symmetry), under progress
  - more realistic grids (from aircraft CAD files)
- ❑ Improve the fan source model, derive a jet noise source model
- ❑ Implement and test a convected wave equation (propagation in uniform flow)
- ❑ Go to higher frequencies : Develop Fast Multipole Method (FMM) (under progress)

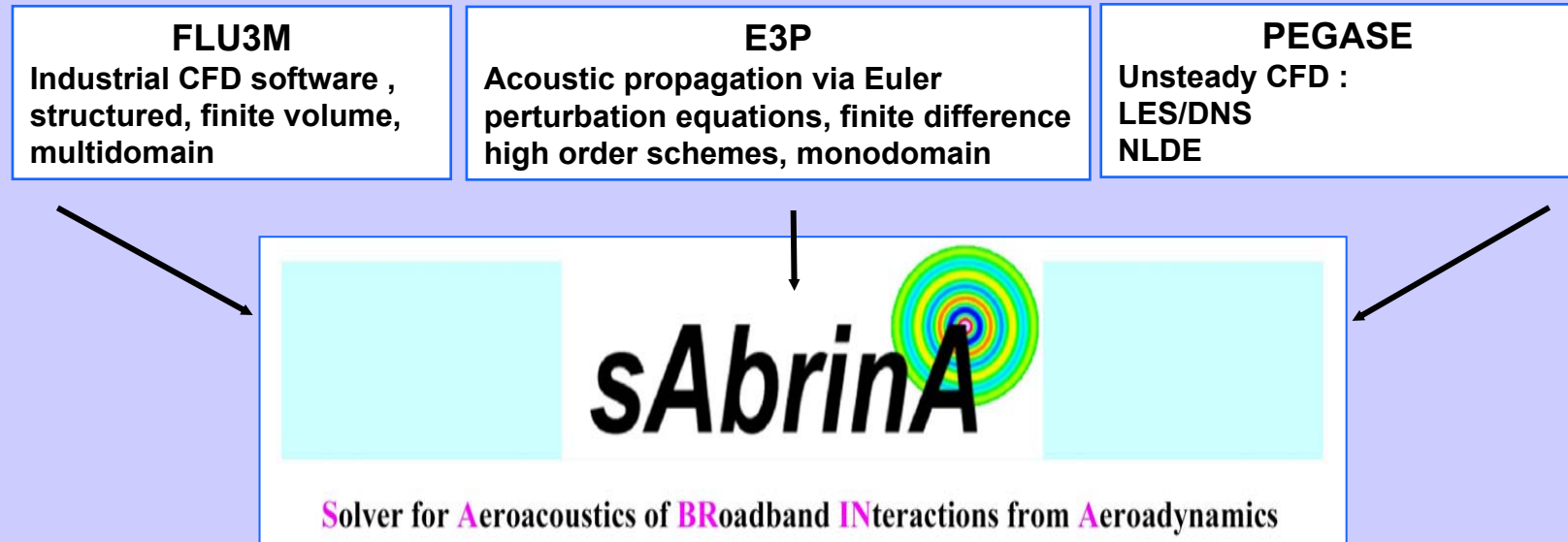
**In-house solvers developed at *ONERA***

***Part II : sAbrinA code***



# *sAbrinA*

*(Solver for Aeroacoustics BRoadband INteractions from Aerodynamics):*  
a 3D multi purposes CFD / CAA code



- Navier-Stokes or non linear Euler equations, in their conservative form
- Complete or Splitted (mean flow / perturbations) variables
- (Explicit, centered) 2<sup>nd</sup> order Finite Volumes or 6<sup>th</sup> order Finite Differences space schemes
- (Explicit) 3<sup>rd</sup> order or (Implicit) 2<sup>nd</sup> order time marching scheme
- (Explicit) 10<sup>th</sup> order filter schemes
- Curvilinear, multi-domains meshes
- Specific (rigid wall, symmetry, periodicity, exit) boundary conditions



## CAA tasks : formulation

Conservative Euler equations

$$\partial_t \mathbf{u} + \nabla \cdot \mathbf{F}(\mathbf{u}) = \mathbf{S}$$

Assuming perfect gas state law and neglecting remote massic forces :

$$\mathbf{u} = \left\{ \begin{array}{c} \rho \\ \rho \mathbf{v} \\ \rho \frac{\mathbf{v}^2}{2} + \frac{1}{\gamma-1} p \end{array} \right\} \quad \mathbf{F}(\mathbf{u}) = \left[ \begin{array}{c} \rho^t \mathbf{v} \\ \rho \mathbf{v} \otimes \mathbf{v} + p \mathbf{I} \\ \left( \frac{\rho \mathbf{v}^2}{2} + \frac{\gamma}{(\gamma-1)} p \right) \left( {}^t \mathbf{v} \right) \end{array} \right] \quad \mathbf{S} = \text{external sources}$$

Mean flow / perturbation splitting :  $\mathbf{u} = \mathbf{u}_p + \mathbf{u}_0$

$\mathbf{u}_p$   
 $\downarrow$   
 Perturbation

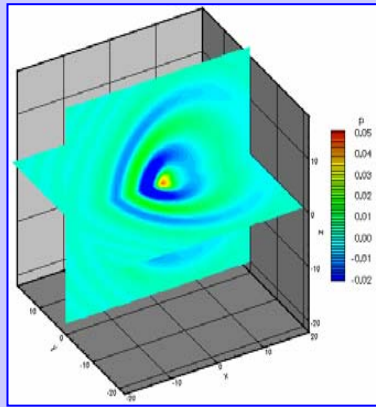
$+$

$\mathbf{u}_0$   
 $\uparrow$   
 Mean flow

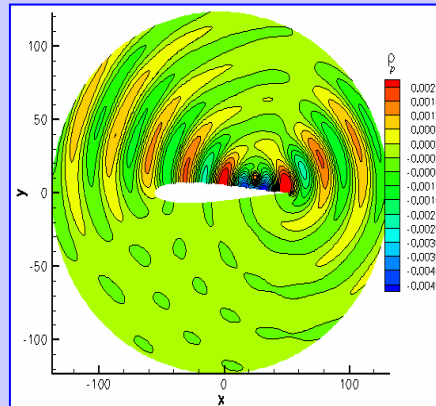
Full (non-linearized) conservative Euler equations

in perturbation formulation :  $\partial_t \mathbf{u}_p + \nabla \cdot [\mathbf{F}(\mathbf{u}_p + \mathbf{u}_0) - \mathbf{F}(\mathbf{u}_0)] = \mathbf{S}$

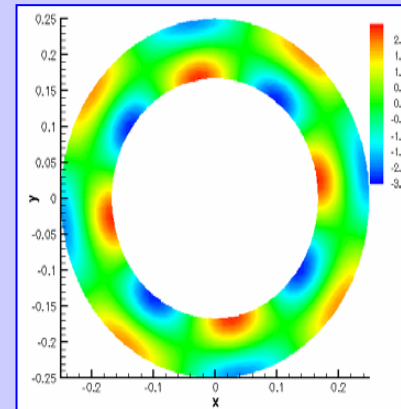
# Validation of *sAbrinA* on CAA complex test cases



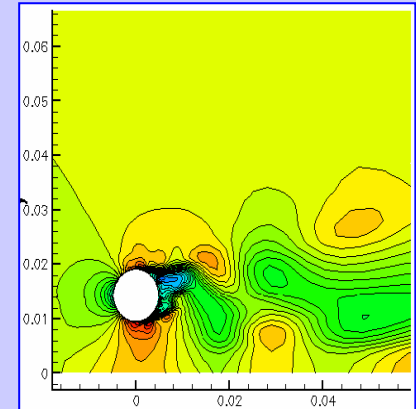
Harmonic source & uniform flow



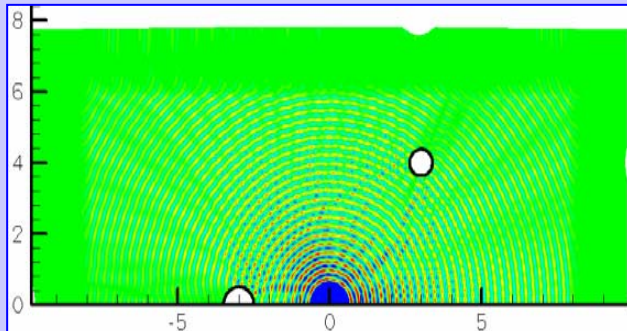
Harmonic source, Joukowski profile



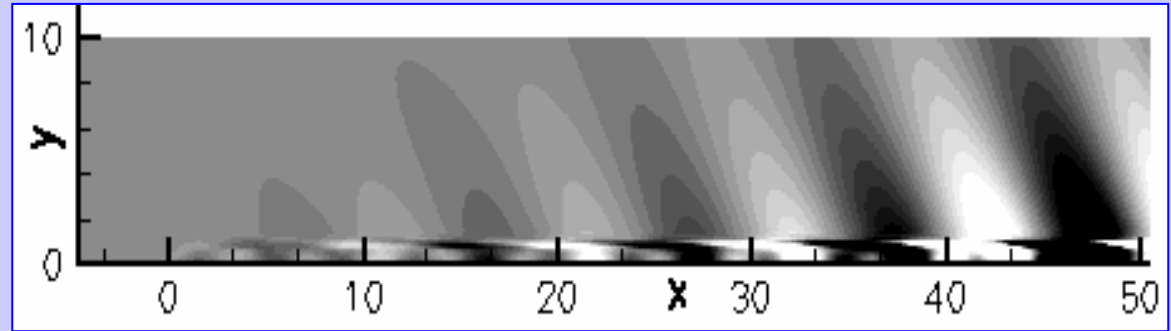
Ducted mode & uniform flow



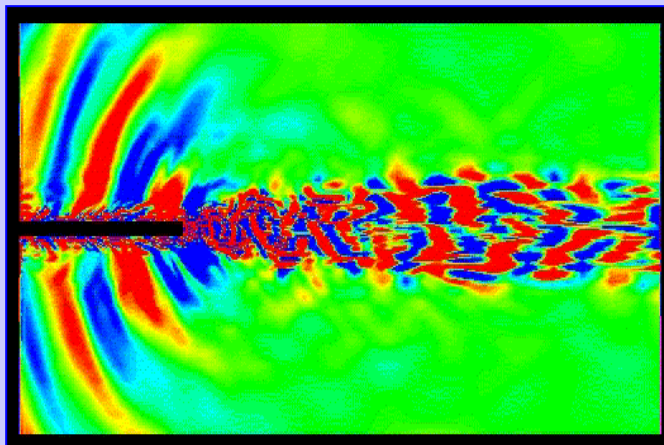
Aeolian tone noise



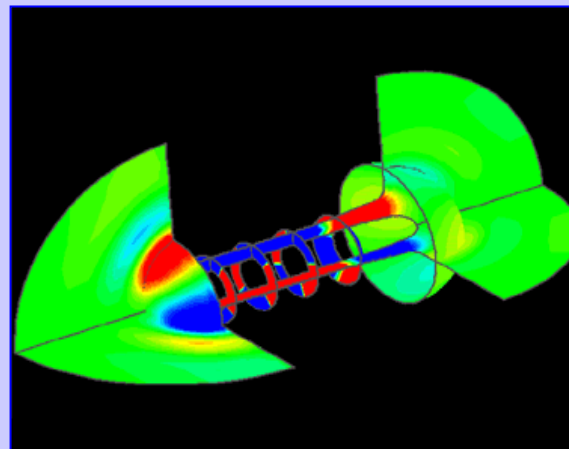
Harmonic source & multiple obstacles



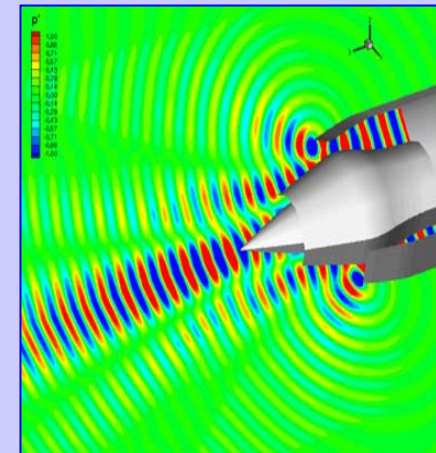
Harmonic source & supersonic shear layer



Trailing edge noise



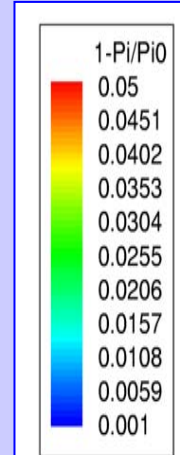
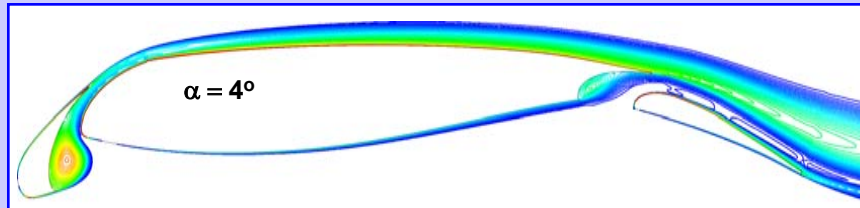
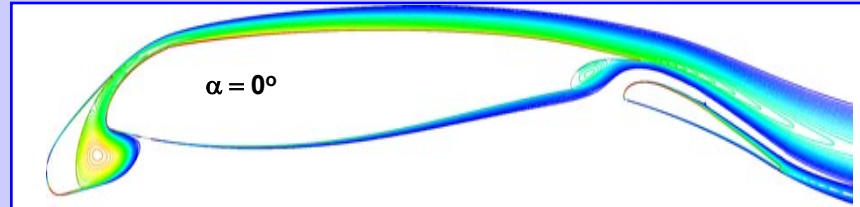
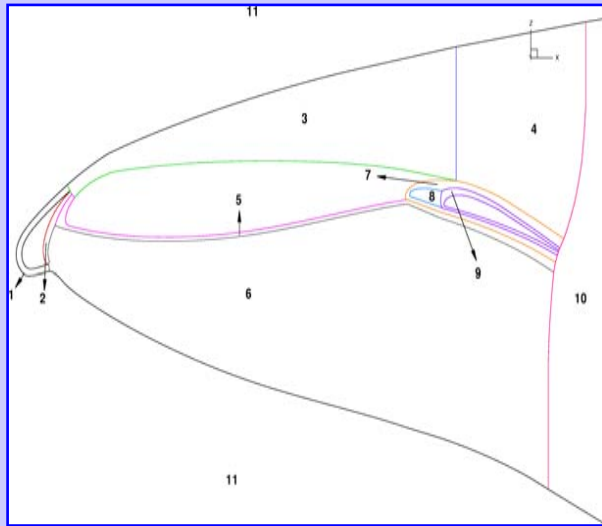
Rotor/stator interaction noise



Downstream fan noise

# Application :

## 2D acoustic scattering from a point source located in the vicinity of a high-lift wing immersed in a non-uniform flow



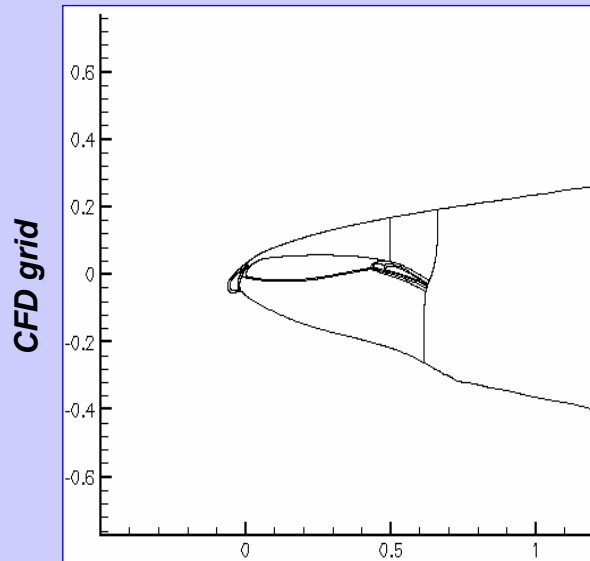
*RANS viscous mean flow grid topology and results ( $0^\circ$  &  $4^\circ$  incidence)*

### CAA computation strategy

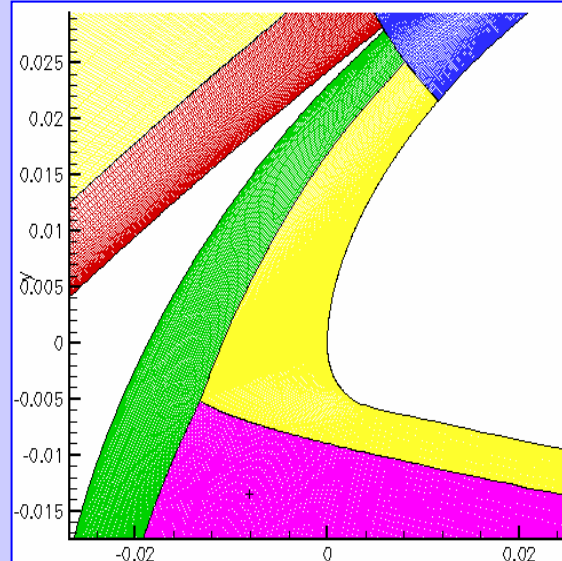
- ☐ Build a homogeneous CAA grid
- ☐ Interpolate the mean flow from CFD to CAA grid
- ☐ Perform 2D CAA computations
  - \* without mean flow (validation vs. BEM)
  - \* with non-uniform mean flow

# CAA grid derivation (R. Guénanff)

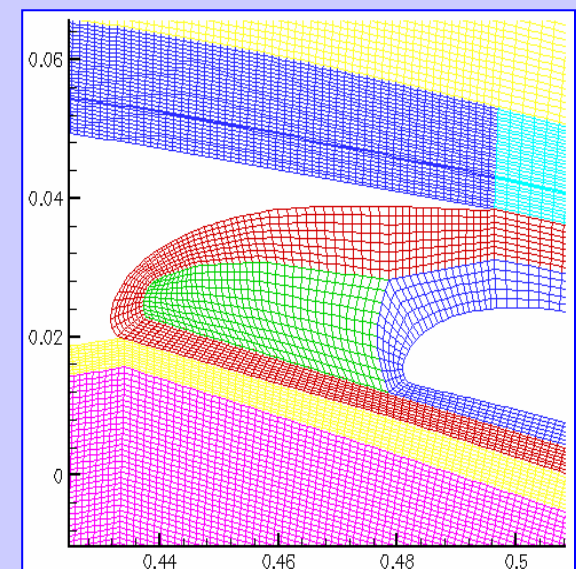
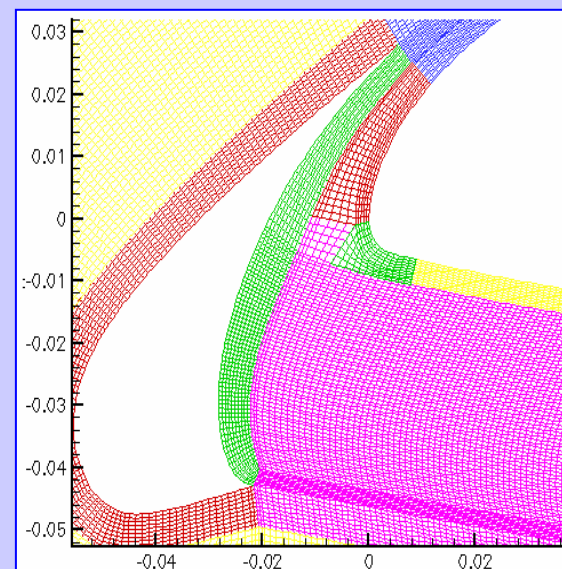
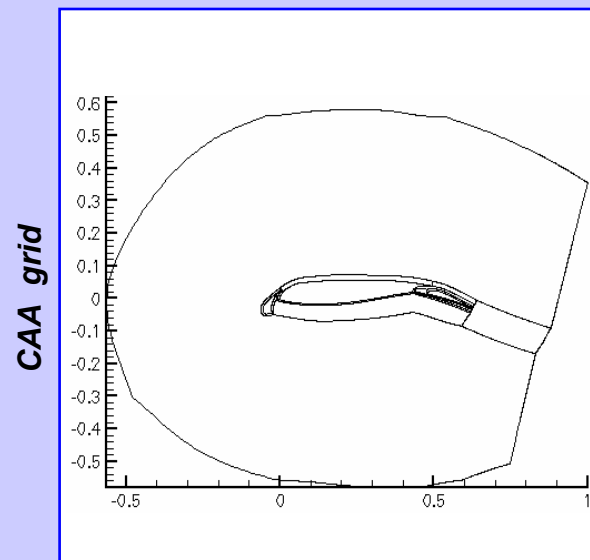
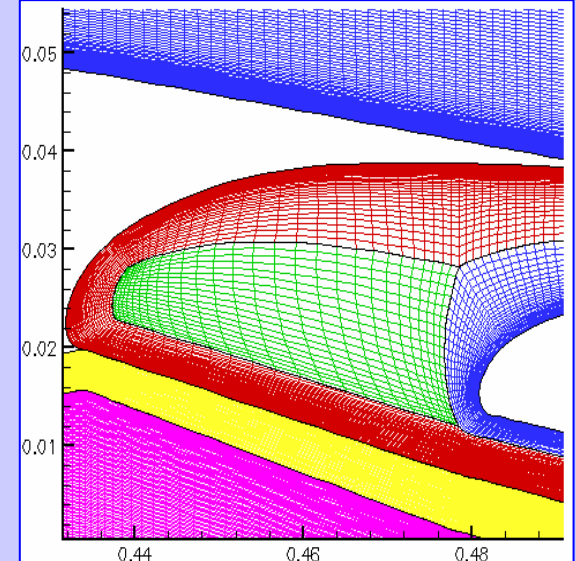
**Blocks structure**



**Slat region**



**Flap region**



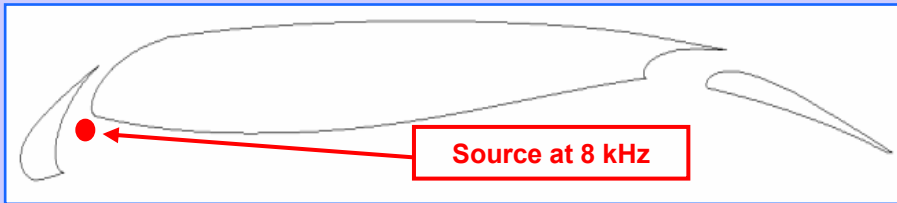
- **Grid adapted up to 30 kHz**
- **Mean flow interpolation from the CFD to the CAA grid : use of TECPLOT routine**



# Early computations (in the context of airframe noise characterization)

## Monopole located inside the slat cove

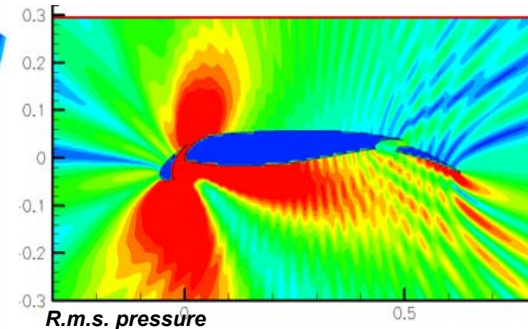
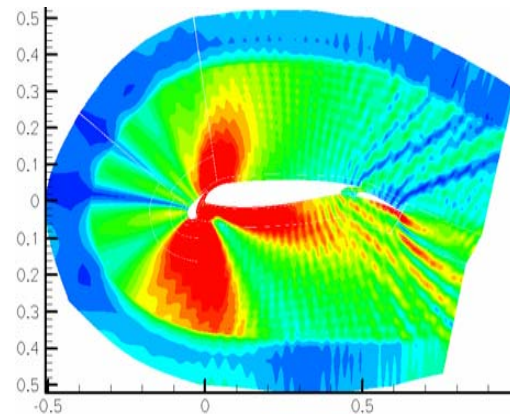
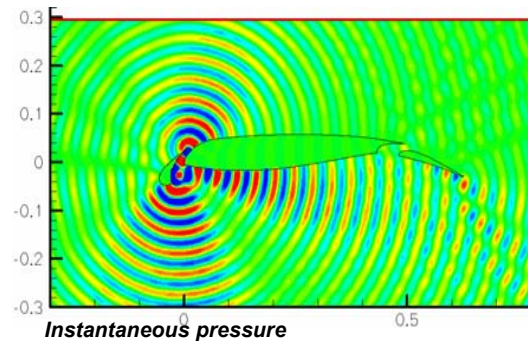
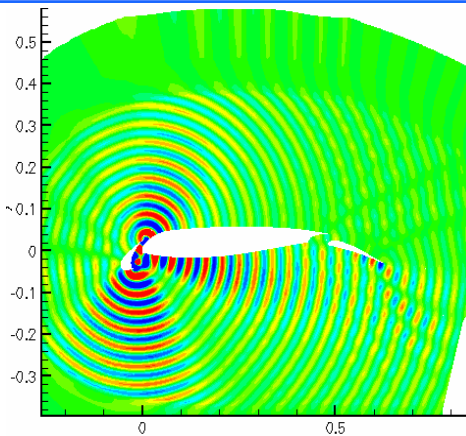
### (1/2) Propagation in a quiescent medium (no flow), and validation against BEM



FD, 6<sup>th</sup> order, RK3

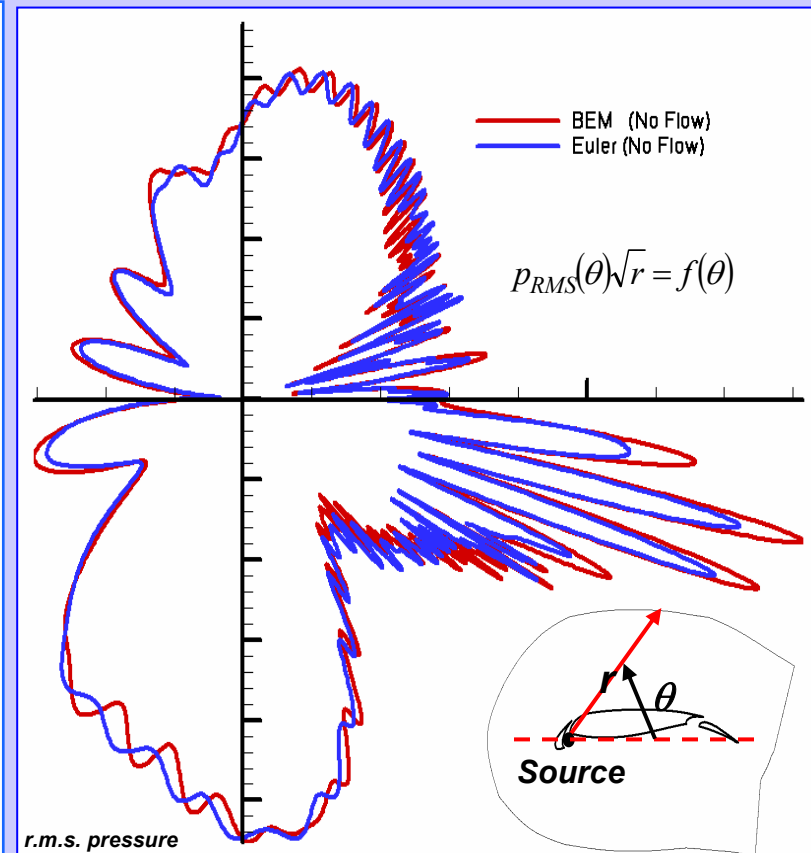
$f = 8 \text{ kHz}$

$\Delta t = 5\text{e-}7 \text{ s } (= T_{\text{source}} / 250), \text{ CFL} = 0.8$



Euler (sAbrinA)

BEM (Sysnoise)

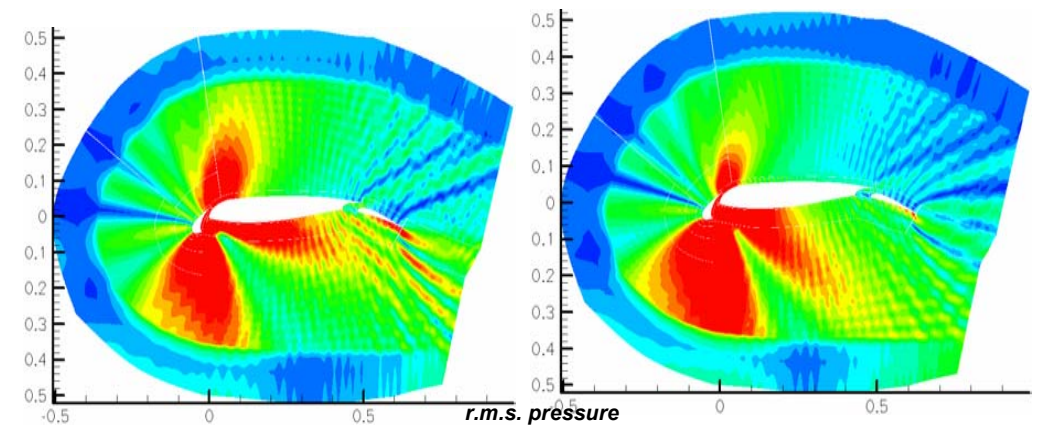
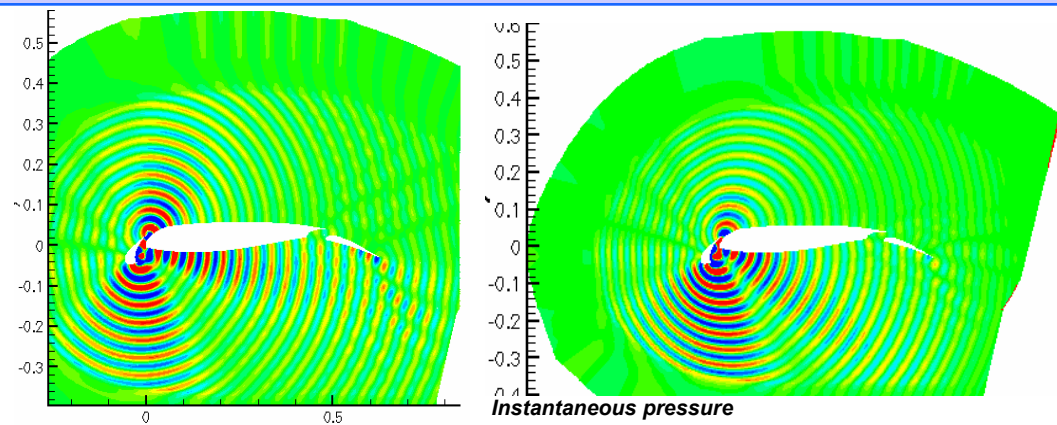


Euler (sAbrinA) vs BEM (Sysnoise)

# Early computations (in the context of airframe noise characterization)

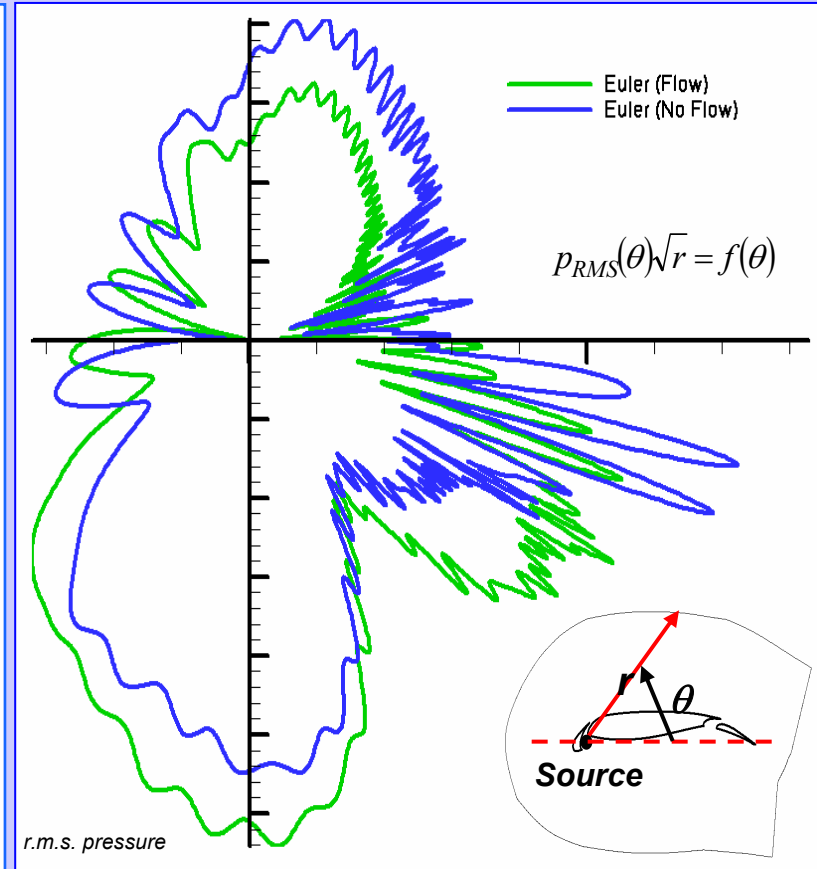
## Monopole located inside the slat cove

### (2/2) Propagation through the non-uniform (RANS) mean flow



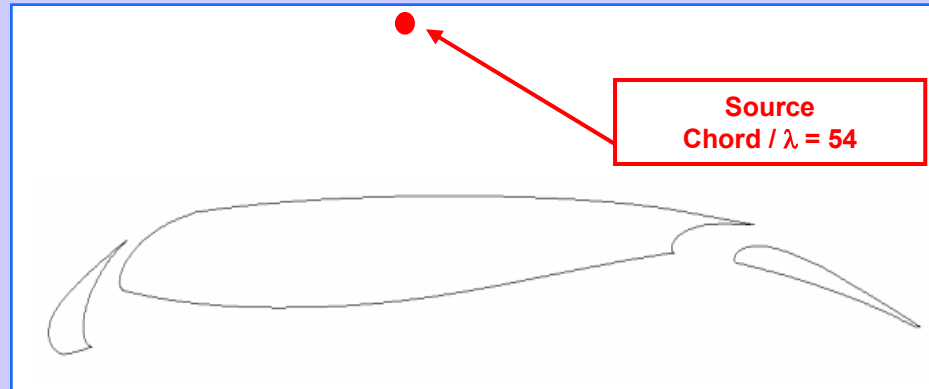
Without mean flow

With non-uniform mean flow



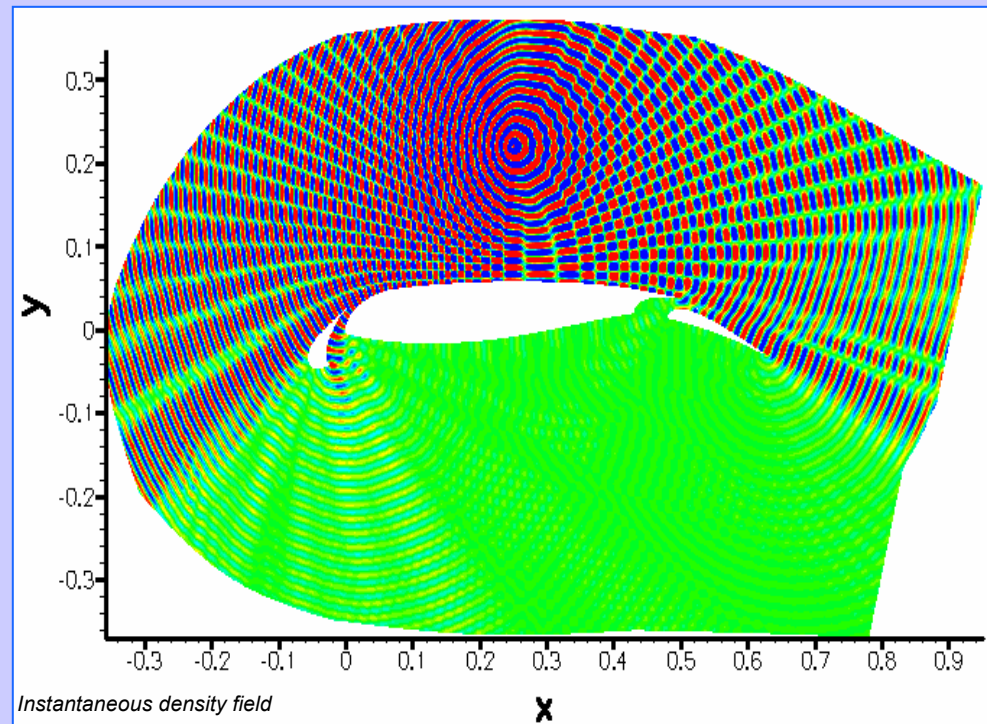
With and without non-uniform mean flow

Application in the context of installation effects  
Monopole located above the suction side  
Propagation in the non-uniform (RANS) mean flow



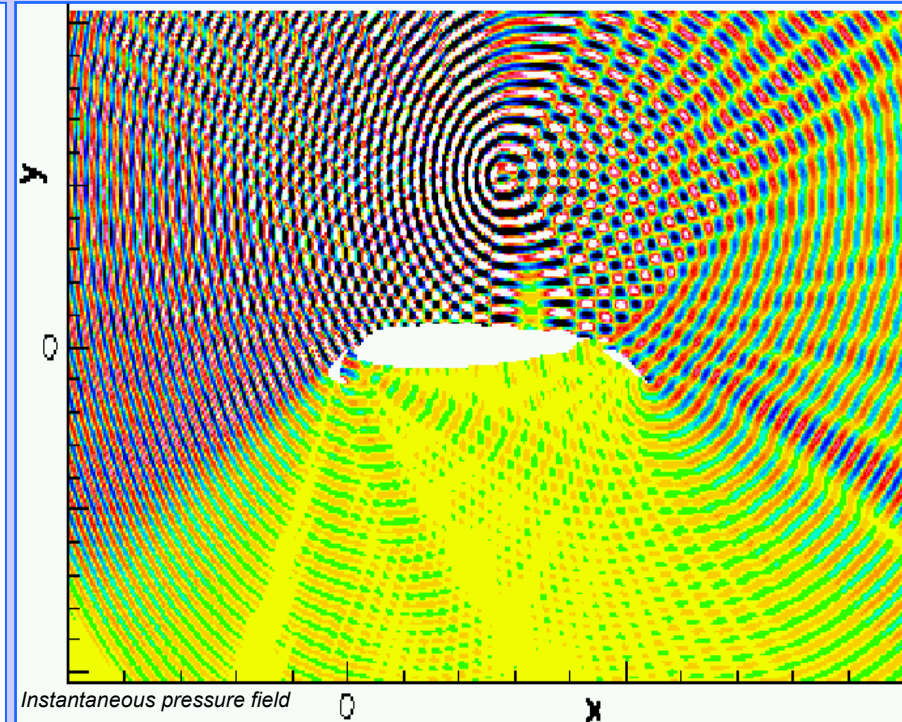
$f = 21 \text{ kHz}$

$f = 16 \text{ kHz}$



Instantaneous density field

*sAbrinA* code



Instantaneous pressure field

*PIANO* code (Roland EWERT, DLR)  
ROSAS benchmark (TCD / DLR / IST)

## ***Application of sAbrina to installation effects studies: Next steps***

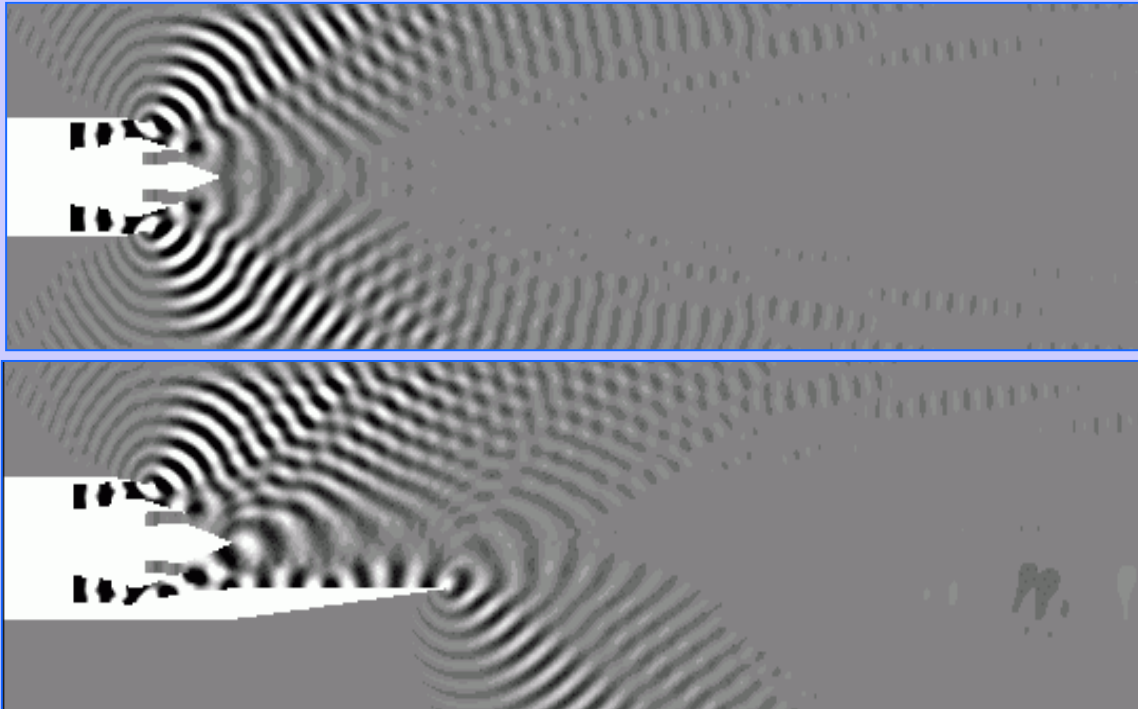
- ☐ **Develop innovative techniques to facilitate complex meshes design (2D, 3D)**
  - ☐ **Non-conformal interface (R. Guénanff PhD thesis)**
  - ☐ **Curvilinear/Cartesian interface (G. Desquesnes PhD thesis)**
- ☐ **Study installation effects on 3D realistic aircraft geometry**
- ☐ **Extend the *sAbrina* capabilities to the treatment of other installation effect configurations**



## Other Installation effects study with sAbrinA

### Numerical Simulation of the Downstream Fan Noise of a Coaxial Jet with a Shielding Surface

by Stéphane REDONNET, Eric MANOHA (ONERA)  
and Owen KENNING (QinetiQ)



Friday 12 November, 11:25

Coming soon...